APPLICATION AND OPERATION OF TWO-STAGE COMPRESSORS

1 General

The two-stage DWM Copeland compressors were developed in order to meet low temperatures required in many of the application areas existing today. They were mainly designed for operation in plants with low evaporation temperatures using R22 or R404A/R507. The distinctive advantage of the application of two-stage compressors is that the operation with R404A allows evaporation temperatures down to ~ -60°C. With single-stage compressors a minimum of ~ -50°C is reached.

Two-stage compressors are divided into the low pressure stage (LP) and the high pressure stage (HP). The 3 cylinder models have two cylinders in the LP and one cylinder in the HP stage; the 6 cylinder models have four cylinders in the LP and two cylinders in the HP stages. Suction gas enters the cylinders of the LP stage where it is compressed to a pressure between the suction pressure and the condensing pressure. This is called intermediate pressure. The gas is then fed from the cylinder heads of the LP stage into the intermediate pressure mixing line. At this point the gas has a relatively high temperature and liquid refrigerant is injected into the gas flow via an expansion valve in order to prevent overheating. The cooled gas flows through the intermediate pressure mixing line arranged externally to the compressor, into the motor housing and the motor, whereby the necessary motor cooling is effected and enters the cylinder of the HP stage in the usual manner where it is compressed to condensation pressure and discharged to the condenser. The discharge from the LP stage into the motor housing and the crankcase are under intermediate pressure. Forced air cooling of the motor and auxiliary ventilation of the cylinder head is not required. Diagrams 1 to 6 show the approximate intermediate pressure (motor housing and crankcase) as well as the temperature under various evaporating and condensing temperatures with R22 and R404A. Refrigeration capacities in the data sheets show the entire refrigeration effect with/or without liquid subcooling, i.e. the product of refrigerant mass flow times the difference of the specific enthalpy of the refrigerant at the inlet of the compressor LP stage and at the outlet of the condenser or liquid subcooler. See diagram 5 without liquid subcooler and diagram 6 with liquid subcooler.

2 Pipe Connections

The connections for high and low pressure switches as well as the discharge and suction shut off valves are located in different positions to those of single-stage compressors. These, and the connections for the intermediate pressure mixing line are shown in Figures 1 to 10 together with the cylinders of the LP and HP stages.

Caution: Never operate a two-stage compressor without the external intermediate pressure mixing line being in position otherwise there is no outlet for the high pressure gas discharged from the low-stage cylinders making an explosive situation.

In the two-stage compressors a Schrader valve is installed to connect a pressure gauge thus enabling easy monitoring of the intermediate pressure. These valves open automatically when the line is connected, using a special coupling. They can be installed subsequently in all compressors which are already in use by removal of the connection plug on the motor side casing over. Schrader valves with 1/8" taper thread 27 NPTF and special connection couplings for them can be supplied by DWM Copeland.
3 Liquid Sub-Cooler

In order to increase the output and the efficiency of the system, a heat exchanger is used as liquid sub-cooler in two-stage compressors and installed between the expansion valve for the intermediate stage and the compressor intermediate pressure mixing line. See figures 7, 8 and 10 showing installation of the subcooler. The evaporated refrigerant first cools the liquid refrigerant on its way to the evaporator and subsequently the discharge gas coming from the cylinders of the low pressure stage. The temperature of the liquid coming from the sub-cooler is about 6K above the saturation temperature of the intermediate stage (saturated temperature corresponding with the intermediate pressure.) The liquid line must be insulated so that the advantages of liquid sub-cooler can be fully utilized. Figures 5 to 10 contain suggestions for plants with and without liquid sub-coolers. When soldering the connections of the sub-cooler, it must be protected against overheating in order to prevent damaging the insulation. If there is a possibility of liquid refrigerant leaving the sub-cooler gaining heat in a long pipe line up to the evaporator expansion valve, then the sub-cooling effect may be lost. In this case, a normal liquid to suction line heat interchanger, available on the open market, should be installed down stream of the evaporator to increase the capacity.

In general the application of liquid to suction heat interchangers at the evaporator outlet and/or the insulation of the suction line reduces or prevents the formation of condensation.

4 Liquid Solenoid Valve

In the liquid line to the intermediate stage, a solenoid valve must be installed directly before the expansion valve to prevent liquid flow during stand still periods. It is electrically connected in such a way that it is open when the motor runs and closed when the motor is off. A manual switch placed in the electric feed line the solenoid valve will facilitate service during pump down. A fine mesh filter also supplied must be installed in the liquid line to the expansion valve for the intermediate stage before the solenoid valve to protect both valves from impurities.

5 Oil Pressure Safety Devices

Oil pressure safety devices are standard equipment of all two-stage compressors. Their use is absolutely necessary. Please see further Technical Bulletins concerning these devices.

6 Oil Separator

As two-stage compressors are especially intended for operation with low evaporation temperatures, oil return from the plant is difficult, and the use of oil separators is mandatory. The oil separator not only reduces the circulating oil flow in the plant but also can act as a muffler and contribute to lower gas pulsations. However, oil separators only have a certain level of efficiency, and some oil will pass over into the low pressure side of the system. The plant must therefore be designed as far as possible to ensure consistent oil return from the suction side. Even this cannot always be achieved, but when for example, after defrosting several times per day the suction pressure at the end of defrost is briefly higher, the gas flow velocity is also higher and oil return can take place.

7 Suction Line Accumulator

In order to prevent damage to these compressors due to refrigerant and/or oil liquid slugging, especially in systems where there is the possibility of liquid or oil being returned to the compressor irregularly, the use of correspondingly dimensioned suction line accumulators is highly recommended. This is especially desirable in the case of two-stage compressors because the suction gas enters directly into the cylinder head. The motor housing, arranged ahead of the high pressure stage, is able to provide a certain separation function. This is only available in the interstage pressure area of two-stage compressors and as a result cannot be effective on the LP suction side. These accumulators must be designed in such a way that constant return of the gaseous refrigerant and oil is guaranteed.

8 Suction Line Filter

Suction line filters should be installed to prevent minute particles of scale, flux, sludge, dirt, copper filings, etc. from entering the compressor.

The selection of the filter must be made very carefully as it creates pressure drop and thus output losses.

9 Liquid Sight Glasses

A liquid line sight glass is supplied and must be installed directly before the intermediate stage expansion valve (de-superheating expansion valve). This enables the liquid supply to be checked.
If a sub-cooler is used a second sight glass should be installed between the receiver and sub-cooler in the main liquid line (figure 7). It should not be installed after the sub-cooler, because due to the sub-cooling the liquid bubbles will not appear, even though a shortage of refrigerant may exist.

10 Relief Valve

In order to protect the crankcase from excessive inter-stage pressure the two-stage compressors are equipped with a relief valve between the intermediate stage and the LP suction chambers. If the inter-stage pressure becomes too high the valve opens a passage to the suction side of the LP stage. The valve is installed in the valve plate on compressor models D6TA/H/J… in the low pressure top cylinder bank). These relief valves open when a differential pressure of 15 bar is exceeded.

11 Suction Pressure Control

During operation of two-stage compressors outside the application limits specified in the technical data sheets, i.e. if the saturation temperature of the suction gas is above the permissible maximum evaporation temperature shown in the technical data sheets, the motor is overloaded and switching off of the motor protector must be taken into consideration. Suction pressure can be limited to a certain maximum value by using a pressure limiting expansion valve (expansion valve with MOP) or by installing a crankcase pressure regulator. The pressure drop in this regulator should correspond to a maximum value of 1K under normal operating conditions.

12 Expansion Valve for Intermediate Stage

In all DWM Copeland two-stage compressors liquid refrigerant is injected via an expansion valve in the inter-stage pressure mixing line in order to decrease the superheat of the discharged gas from the low pressure stage. The expansion valves which are a part of the equipment of two-stage compressors are shown in Table 1 & 2. For 3 cylinder version “3” compressors non adjustable valves are standard delivery. For 4 & 6 cylinder compressors adjustable valves are used.

If the expansion valve does not function properly, check to determine whether this valve, the solenoid valve or the filter in the liquid line are blocked. The latter must be cleaned. The expansion valve must be flushed through thoroughly. If despite cleaning no satisfactory result has been reached, the valve must be changed. In case that the superheat of the valves has to be controlled or corrected see Table 1 & 2 and/or following recommendations:

Normally it will be necessary to control and alter the factory adjustment of the adjustable valve in order to achieve the corresponding output. The valve must be set in such a way that the temperature difference (superheat) of 8K to 16K is reached between the temperature of the inter-stage pressure line at the bulb and the saturation temperature of refrigerant under inter-stage pressure (gauge pressure reading).

Example

Use of R 22 with an inter-stage pressure of 3.19 bar (a)

<table>
<thead>
<tr>
<th>Required super-heating limitation at 3.19 bar (a)</th>
<th>8K</th>
<th>16K</th>
</tr>
</thead>
<tbody>
<tr>
<td>Saturation temperature</td>
<td>-13°C</td>
<td>-13°C</td>
</tr>
<tr>
<td>Resulting temperature</td>
<td>-5°C</td>
<td>3°C</td>
</tr>
</tbody>
</table>

The expansion valve for the intermediate stage must therefore be adjusted in such a manner that a temperature in the inter-stage pressure mixing line at the bulb is maintained between -5 °C and +3°C.

The following tables 1 & 2 are showing the de-superheating expansion valves for inter-stage injection, as well as the DWM Copeland Part Number with the relevant Sporlan or Alco model (adjustable or non-adjustable) for the corresponding compressor models. Subcoolers are also listed.

With adjustable de-superheating expansion valves superheating can be increased by rotating the superheat adjustment screw in a clockwise direction and decreased by rotating counter clockwise. Instructions for readjustment of the adjustable valves apply to the standard application range (see data sheet).
Our tests have shown that the same expansion valve for both R22 and R404A can be used with satisfactory results (approved compressors: see literature).

When using the compressors outside of the application limits specified in the technical data sheets, i.e. for R22 down to approximately -60°C and for R404A down to approximately -70°C evaporation temperature the use of such an adjustable expansion valve is necessary and must be adjusted. Wide fluctuation in pressure, caused by opening and closing of the expansion valve must be avoided. Superheating at the valve bulb is between 8 and 16K. False adjustment or malfunction of the expansion valve can lead to a return of liquid refrigerant in the motor and crankcase which among other things can cause oil dilution.

For operation of the compressor outside of the application limits specified by DWM Copeland the agreement of the Application Engineering department should be obtained.

**NOTE:** The connection of the liquid line to the expansion valve for the intermediate stage must be made very carefully. The line may not be smaller than 10 mm o.d. and must be connected to a horizontal line from below so that a constant liquid flow is ensured at all times. This line must never originate on the top of a horizontal line because then only gas may flow. In this case the temperature in the intermediate pressure mixing line would be too high and the motor would not be sufficiently cooled. Connection to a vertical line with low velocity is permissible.

### 13 Twin Operation

The Twin combination of two-stage compressors via connection of their motor sides by means of an intermediate manifold and allows if needed part-load operation (cycling one compressor from the Twin on & off). It is recommended to use one oil separator for each compressor. Further for two-stage Twin-compressors a connection line between the pressure shut off valves (HP side) must be provided on site. There is an external connecting line between the suction shut-off valves that is part of the scope of delivery for 6 cylinder twin compressors only. In each case the discharge line must be installed downward from the shut off valve in order to ensure that the oil is not forced from one operating compressor to the other compressor at standstill. An obligatory example of installation schemes for two-stage Twin compressors can be found on pages 14 and 15 figures 9 & 10.

Please note also that the Twin-compressor is mounted on its frame by means of employing rubber shims to equalize the manufacturing tolerances and to avoid stress that may arise during the installation of the Twin compressor. If the foundation base is light and if sound and vibration transmission have to be reduced additional absorbers should be installed between the frame and the foundation (installation on site).

In case that only one compressor of the Twin is operating it has to be ensured that the de-superheating expansion valve of this specific compressor is fed with liquid refrigerant so that the de-superheating of the inter-stage gas is working properly.

To ensure that the obtained liquid subcooling / cooling capacity is not wasted, the system has to be designed correctly. Also make sure that no hydrostatic pressure can occur in parts of the system, e.g. separated by magnetic valves.
14 Unloaded Start

For the prevention of system disturbances power companies limit the permissible size of motor for Direct-On-Line starting. A substantial reduction of the breakaway motor starting current can only be achieved if the load on the motor is reduced at the same time. Various starting methods are available like Star-Delta, Part Winding, Resistance, Phase Angle Control (Soft-starting) or Transformer Start.

In general an unloaded start (bypass) of the compressor is also necessary additional to the pre-mentioned starting methods. This is achieved by connecting the HP discharge side with the LP suction side of the compressor on site by means of a bypass line with solenoid valve. The discharge gas is returned to the suction side of the compressor thus equalizing the pressures across the compressor for starting. A check valve in the discharge line is also necessary.

While selecting and installing please observe Section 16 concerning discharge pulsation, chattering of the check valve due to pulsation must be avoided.

The unloaded start equipment offered by DWM Copeland for single-stage compressors is not suitable for two-stage compressors. Some basic recommendations concerning typical wiring of two-stage compressors are shown on pages 16 & 17.

15 Defrost Equipment

15.1 Electric

With electric defrost equipment, the compressor is not in operation during the defrost cycle, thus no special precautionary measures are necessary in addition to the normal measures for single-stage systems.

15.2 Hot Gas

In two-stage compressors the motor cooling depends on the adequate supply of liquid refrigerant for the expansion valve for the intermediate stage. If hot-gas defrost equipment is used it is absolutely necessary that a sufficient amount of liquid with sufficient pressure is supplied to the expansion valve at all times. As hot gas defrost equipment vary widely in design it is not possible to establish general rules on which special monitoring devices are necessary. Many manufacturers have tested their devices thoroughly; during application of the defrost, however, throttle valves may be necessary to maintain the liquid pressure together with additional refrigerant charge or other special monitoring equipment.

16 Pulsation/Vibrations

All reciprocating compressors cause gas pulsation in the discharge line. The intensity of the pulsation increase with the decreasing number of cylinders, which discharge into a common discharge line and with the increase of volume and density of the supplied gas.

Two-stage compressors operate with gas of higher density in the HP stage. In compressor models D9 only one cylinder and D6 two cylinders discharge into the discharge line therefore the pulsation of two-stage compressors can be larger than that of single-stage compressors.

Normally these pulsation do not create any problems. Sometimes, however, the combined reaction of operating conditions, mounting and pipe arrangement can result in a resonant condition, which tends to magnify the pulsation and cause vibration.

In order to solve this problem muffler plates for D9 and D6 two-stage compressors have been developed. These muffler plates fit between the compressor casing and the discharge shut off valve. These plates give an effective dampening of compressor pulsations. They are now being installed in all new two-stage compressors as standard equipment. If pulsation problems exist in already operating systems, the installation of muffler plates is recommended. These plates are available from us under the part number listed in our spare parts list.

If the size of pipes and connections are such that resonance is created and the muffler plate does not dampen it sufficiently, it may be necessary to bolt the compressor to the supporting base with rubber vibration dampers, whereby vibration frequency is altered. Top and bottom vibration damper can be found in our spare parts list.
Inter-stage Expansion Valves and Liquid Subcoolers

| Compressor Model | Subcooler (separate) | Interstage TXV  
<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>Variation 3</td>
<td>Co-axial HX to be fitted on site</td>
<td>(can also be used on a compressor without subcooler)</td>
</tr>
<tr>
<td>Valid until Feb. 2001</td>
<td>With Internal Pressure Equalisation</td>
<td></td>
</tr>
<tr>
<td>Part Number of Subcooler</td>
<td>Type</td>
<td>Part Number</td>
</tr>
<tr>
<td>D9TK3 - 0760</td>
<td>D9TL3 - 0760</td>
<td>Sporlan NIV-2-Z,32 psig</td>
</tr>
<tr>
<td>D9TH3 - 0760</td>
<td>Sporlan NIV-3-Z,37 psig</td>
<td>2051004</td>
</tr>
<tr>
<td>D9TH3 - 1010</td>
<td>Sporlan NIV-3-Z,32 psig</td>
<td>2502455</td>
</tr>
</tbody>
</table>

| | | | | | |
| | | | | | |
| | | | | | |

| Compressor Model | Subcooler (mounted) | Interstage TXV  
<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>Variation 4</td>
<td>Plate HX</td>
<td>(can also be used on a compressor without subcooler)</td>
</tr>
<tr>
<td>From Mar. 2001</td>
<td>With External Pressure Equalisation</td>
<td></td>
</tr>
<tr>
<td>Part Number of Subcooler</td>
<td>Adjustable Type &amp; Part Number</td>
<td></td>
</tr>
<tr>
<td>D9TK4 - 0760</td>
<td>D9TL4 - 0760</td>
<td>Sporlan BFV-C-C 6611048 (for use with subcooler)</td>
</tr>
<tr>
<td>D9TH4 - 0760*</td>
<td>D9TH4 - 1010</td>
<td>Sporlan BFV-C-C 6611037 (for use with subcooler)</td>
</tr>
<tr>
<td>2979360</td>
<td>ALCO TCLE-GT 2744 (Pre-set) 2979371</td>
<td></td>
</tr>
</tbody>
</table>

Table 1: Three Cylinder Two-Stage Compressor - R22 only

**NOTE:** Compressor model designation varies with type of subcooler and interstage expansion valve. Do not use interstage expansion valves with internal pressure equalisation with plate heat exchangers

* Model phased out January 2005

<table>
<thead>
<tr>
<th>Compressor Models</th>
<th>Plate HX Subcooler</th>
<th>Interstage TXV</th>
</tr>
</thead>
<tbody>
<tr>
<td>D6TA - 1500/X</td>
<td>Spare Part No. 6611253</td>
<td>With external pressure equalisation Sporlan BFVECC 6611048 (for use with subcooler)</td>
</tr>
<tr>
<td>D6TH - 2000/X</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D6TJ - 2500/X</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>With internal pressure equalisation Sporlan BFV-C-C 6611037 (for use with subcooler)</td>
<td></td>
</tr>
</tbody>
</table>

Table 2: Six Cylinder Two-Stage Compressor - R22 & R404A

**NOTE:** The "X" in compressor model designation indicates compressor filled with ester oil. The D6T* compressors arrive with HX as a part of the standard delivery. Without HX is an option.

Standard delivery: with HX and TXV (non adjustable before February 2001).
Diagram 1

3 cylinder two-stage compressor without subcooler, R22

Diagram 2

3 cylinder two-stage compressor with subcooler, R22
Diagram 5

6 cylinder two-stage compressor without subcooler, R404A

Diagram 6

6 cylinder two-stage compressors with subcooler, R404A
Figure 1: 3 cylinder two-stage compressor (Version D9T.3..) without liquid subcooler - connections

Liquid subcooler (separate for D9T.3
Connections to be installed on field

Figure 2: 3 cylinder two-stage compressor (Version D9T.4..) with liquid subcooler mounted at compressor connections

SL = Suction shut-off valve
DL = Discharge shut-off valve
E.V. = De-superheating expansion valve
1 = plug low-pressure connection
2 = plug high-pressure connection
3 = plug oil charge
4 = flare oil-pressure control H.P.
5 = plug oil-pressure control L.P.
6 = oil-pressure connection (Schrader)
7 = oil screen (internal)
8 = sleeve (crankcase heater )
9 = intermediate pressure connection (Schrader)
10 = magnetic plug
11 = liquid line to evaporator, sweat
12 = connection de-superheating expansion valve
13 = line to compressor interstage manifold, sweat
14 = liquid line from receiver, sweat
15 = insulation
16 = plug oil-pressure sensor
17 = plug intermediate pressure connection
18 = plug oil-pressure control
19 = solenoid valve
20 = liquid subcooler
21 = filter
22 = sight glass
23 = sight glass
24 = sight glass
25 = sight glass
26 = sight glass
Figure 3: 6 cylinder two-stage compressor without liquid subcooler connections Models with flat bottom plate shown

Figure 4: 6 cylinder two-stage compressor with liquid subcooler mounted at compressor-connections

SL = Suction shut-off valve
DL = Discharge shut-off valve
E.V. = De-superheating expansion valve
1 = plug low-pressure connection
2 = plug high-pressure connection
3 = plug oil charge
4 = flare oil-pressure control H.P.
5 = plug oil-pressure control L.P.
6 = oil-pressure connection (Schrader)
7 = oil screen (internal)
8 = plug or sleeve (crankcase heater)
9 = intermediate pressure connection
9a = intermediate pressure connection (Schrader)
10 = magnetic plug
21 = liquid line to evaporator, sweat
22 = liquid line from receiver, sweat
16 = insulation
17 = plug oil-pressure sensor
20 = liquid subcooler
24 = filter
25 = solenoid valve
26 = sight glass
Figure 5: System with 3 cylinder two-stage compressor without liquid subcooler

Figure 6: System with 6 cylinder two-stage compressor without liquid subcooler

53 = condenser
54 = receiver
55 = evaporator
56 = suction line (LP)
57 = interstage line (insulated)
58 = liquid line to thermostatic expansion valve 63a
to be connected to main liquid line
59 = discharge line (HP)
60 = oil separator (close to compressor)
61 = oil return line to compressor
62 = suction accumulator (with built-in oil return)
sized according to maximum Refrigerant charge
63 = thermostatic expansion valve at evaporator
63a = thermostatic expansion valve interstage injection
64 = bulb location for thermostatic expansion valve
65 = solenoid valve in liquid line (only open during compressor operation)
65a = solenoid valve in bypass for unloaded start
66 = sight glass
67 = filter (drier)
68 = low pressure connection
69 = discharge line (HP)
70 = oil separator (close to compressor)
71 = oil return line to compressor
72 = suction accumulator (with built-in oil return)
sized according to maximum Refrigerant charge
73 = thermostatic expansion valve at evaporator
74 = thermostatic expansion valve interstage injection
75 = bulb location for thermostatic expansion valve
76 = solenoid valve in liquid line (only open during compressor operation)
77 = solenoid valve in bypass for unloaded start
78 = sight glass
79 = filter (drier)
80 = low pressure connection
81 = discharge line (HP)
Figure 7: System with 3 cylinder two-stage compressor (Version D9T. 3..) with liquid subcooler (separate)

Figure 8: System with 6 Cylinder two-stage compressor with liquid subcooler (mounted at compressor)

52 = heat-exchanger (liquid-subcooler)  
53 = condenser , 54 = receiver  
55 = evaporator  
56 = suction line (LP)  
57 = interstage line (insulated)  
58 = liquid line to thermostatic expansion valve 63a to be connected to main liquid line  
59 = discharge line (HP)  
60 = oil separator (close to compressor)  
61 = oil return line to compressor  
62 = suction accumulator (with built in oil return) sized according to maximum refrigerant charge  
63 = thermostatic expansion valve at evaporator  
63a = thermostatic expansion valve interstage injection  
64 = bulb location for thermostatic expansion valve  
65 = solenoid valve in liquid line (only open during compressor operation)  
65a = solenoid valve in bypass for unloaded start  
66 = sight glass  
67 = filter (drier)  
68 = low pressure connection  
69 = high pressure connection  
70 = intermediate pressure connection  
71 = plug high pressure connection  
72 = insulation  
73 = check valve to be sized correctly in order to avoid noise from chattering  
74 = vibration absorber  
75 = shut-off valve  
76 = filter  
77 = loop for flexibility  
78 = bypass for unloaded start
Figure 9: System with 6 cylinder two-stage Twin-compressor without liquid subcooler

53 = condenser
54 = receiver
55 = evaporator
56 = suction line (LP)
57 = interstage line (insulated)
58 = liquid line to thermostatic expansion valve 63a to be connected to main liquid line
59 = discharge line (HP)
60 = oil separator (close to compressor)
61 = oil return line to compressor
62 = suction accumulator (with built-in oil return) sized according to maximum refrigerant charge
63 = thermostatic expansion valve at evaporator
63a = thermostatic expansion valve interstage injection
64 = bulb location for thermostatic expansion valve
65 = solenoid valve in liquid line (only open during compressor operation)
66 = sight glass
67 = filter (drier)
68 = low pressure plug
70b+c = intermediate pressure connections
72 = insulation
73 = check valve to be sized correctly in order to avoid noise from chattering
74 = heat exchanger (suction/liquid)
77 = vibration absorber
78 = shut-off valve
79 = filter
80 = loop for flexibility
81 = bypass for unloaded start
82 = e.g. room-thermostat
83 = suction header
Figure 10: System with 6 cylinder two-stage Twin-compressor with liquid subcooler

52 = liquid subcooler
53 = condenser
54 = receiver
55 = evaporator
56 = suction line (LP)
57 = interstage line (insulated)
58 = liquid line to thermostatic expansion valve 63a
59 = discharge line (HP)
60 = oil separator (close to compressor)
61 = oil return line to compressor
62 = suction accumulator (with built-in oil return)
   sized according to maximum refrigerant charge
63 = thermostatic expansion valve at evaporator
63a = thermostatic expansion valve interstage injection
64 = bulb location for thermostatic expansion valve
65 = solenoid valve in liquid line (only open during compressor operation)
66 = sight glass
67 = filter (drier)
69 = low pressure plug
70b+c = intermediate pressure connection
72 = insulation
73 = check valve to be sized correctly in order to avoid noise from chattering
77 = vibration absorber
78 = shut-off valve
79 = filter
80 = loop for flexibility
81 = bypass for unloaded start
82 = e.g. room-thermostat
83 = suction header
**Figure 11:** Schematic wiring diagram for Two–Stage compressors Y / Δ Start with unloading device

- **Q1** = main switch
- **S1** = auxiliary switch, when crankcase heater is to heat prior to starting the compressor
- **K1** = compressor motor contactor
- **K2** = star contactor for compressor motor
- **K3** = delta-contactor for compressor motor
- **K11** = time delay relay for change over of the motor from star to delta (1-3 seconds)
- **F1** = fuse for control circuit (characteristics according to maximum load of contacts of control devices)
- **A1** = module motor protection
- **F3..32** = pressure cut out (according to local regulations)
- **A2** = oil pressure safety control system OPS1
- **F6** – **F8** = fuses
- **B1** = room thermostat
- **M1** = compressor motor
- **Y3** = solenoid valve for unloaded start Fig.11
- **Δ p** = pressure difference switch for A2
Figure 12: Schematic wiring diagram for Two–Stage compressors Part Winding Start with unloader

K4 = Contactor for second winding of part-winding motor
K12 = Time delay relay for second part-winding 1sec.( +/- 0,1)
R2 = Crankcase heater
R5 = Sensors in the compressor motors- must be connected to the electronic module A1
Y1 = Solenoid valve for liquid line
Y4 = Solenoid valve inter-stage liquid line
A1 = Electronic module, system W
A2 = Oil pressure difference control system OPS1
H1 = Signal lamp

Information in this document are subject to change without notification.